

D3

PCT

WORLD INTELLECTUAL PROPERTY ORGANIZATION  
International Bureau



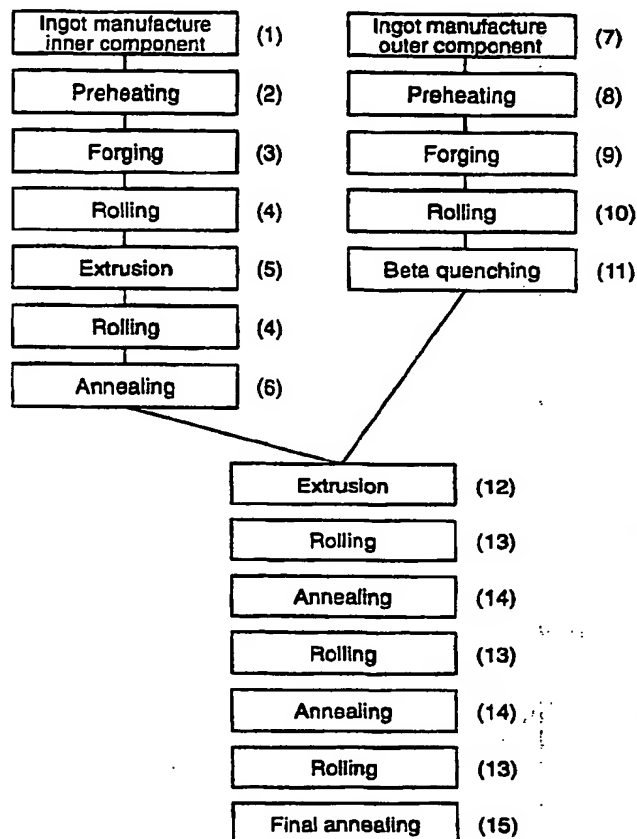
INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

(51) International Patent Classification <sup>5</sup> : <b>G21C 21/02, 3/20</b>		A1	(11) International Publication Number: <b>WO 94/15343</b>
			(43) International Publication Date: <b>7 July 1994 (07.07.94)</b>
(21) International Application Number: <b>PCT/SE93/01070</b>			(81) Designated States: FI, JP, US, European patent (AT, BE, CH, DE, DK, ES, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE).  <b>Published</b> <i>With international search report.</i> <i>With amended claims.</i> <i>In English translation (filed in Swedish).</i>
(22) International Filing Date: <b>15 December 1993 (15.12.93)</b>			
(30) Priority Data: <b>9203871-0</b> <b>18 December 1992 (18.12.92)</b> <b>SE</b>			
(71) Applicant (for all designated States except US): <b>ABB ATOM AB [SE/SE]; S-721 63 Västerås (SE).</b>			
(72) Inventor; and (75) Inventor/Applicant (for US only): <b>DAHLBÄCK, Mats [SE/SE]; Mangelgatan 13, S-724 76 Västerås (SE).</b>			
(74) Agent: <b>LUNDBLAD VANNESJÖ, Katarina; ABB Corporate Research, Patent Department, S-721 78 Västerås (SE).</b>			

(54) Title: **MANUFACTURE OF ZIRCONIUM CLADDING TUBE WITH INTERNAL LINER**

(57) Abstract

A method of manufacturing nuclear fuel elements comprising fuel rods whose cladding tubes are provided with an internal liner layer to obtain PCI resistance in the nuclear fuel element comprises carefully choosing parameters for heat treatment of the inner component even from the machining of an ingot of the inner component. The internal layer of zirconium or a zirconium alloy suitable as inner layer in a PCI-resistant cladding is manufactured, from the fabrication of an ingot of the inner component up to the completion of a cladding tube, comprising forging, rolling, extrusion, heat treatment and final heat treatment, in such a way that the temperature in the inner component never exceeds the temperature when an incipient phase transformation to beta phase takes place.



**FOR THE PURPOSES OF INFORMATION ONLY**

Codes used to identify States party to the PCT on the front pages of pamphlets publishing international applications under the PCT.

AT	Austria	GB	United Kingdom	MR	Mauritania
AU	Australia	GE	Georgia	MW	Malawi
BB	Barbados	GN	Guinea	NE	Niger
BE	Belgium	GR	Greece	NL	Netherlands
BF	Burkina Faso	HU	Hungary	NO	Norway
BG	Bulgaria	IE	Ireland	NZ	New Zealand
BJ	Benin	IT	Italy	PL	Poland
BR	Brazil	JP	Japan	PT	Portugal
BY	Belarus	KE	Kenya	RO	Romania
CA	Canada	KG	Kyrgyzstan	RU	Russian Federation
CF	Central African Republic	KP	Democratic People's Republic of Korea	SD	Sudan
CG	Congo	KR	Republic of Korea	SE	Sweden
CH	Switzerland	KZ	Kazakhstan	SI	Slovenia
CI	Côte d'Ivoire	LI	Liechtenstein	SK	Slovakia
CM	Cameroon	LK	Sri Lanka	SN	Senegal
CN	China	LU	Luxembourg	TD	Chad
CS	Czechoslovakia	LV	Latvia	TG	Togo
CZ	Czech Republic	MC	Monaco	TJ	Tajikistan
DE	Germany	MD	Republic of Moldova	TT	Trinidad and Tobago
DK	Denmark	MG	Madagascar	UA	Ukraine
ES	Spain	ML	Mali	US	United States of America
FI	Finland	MN	Mongolia	UZ	Uzbekistan
FR	France			VN	Viet Nam
GA	Gabon				

Manufacture of zirconium cladding tube with internal liner

## TECHNICAL FIELD

5 The present invention relates to a method of manufacturing a nuclear fuel element comprising fuel rods the cladding tubes of which are provided with an internal liner of zirconium or a zirconium alloy.

## 10 BACKGROUND ART

A nuclear fuel element comprises fuel rods with cladding tubes filled with fuel pellets. It is known to provide cladding tubes with an internal layer of zirconium or a  
15 zirconium alloy to protect the fuel element from destruction caused by pellet-clad interaction, PCI, in case of rapid power increases.

SE 7810262 describes a nuclear fuel element with improved  
20 properties regarding the resistance to PCI and comprising a composite cladding container comprising an outer part of a zirconium alloy and an inner part, bonded to the outer part and consisting of zirconium with an impurity content of about 1000 to 5000 ppm.

25 This composite cladding tube is manufactured by inserting a sleeve of sponge zirconium, which is to be used as internal part, into a hollow billet of a zirconium alloy which is to constitute the outer part, whereupon the unit is subjected  
30 to explosion bonding of the sleeve to the billet. Thereafter, the composite product is extruded at a temperature of about 538 - 750°C while using conventional extrusion methods. Thereafter, the extruded composite product is sub-  
35 jected to a conventional tube production until the desired dimension of the cladding has been reached. The bond of the sleeve to the billet can also take place by means of heating to 750°C for 8 hours to achieve a diffusion bond. The manufacture of the composite cladding can also take place by

extruding the unit, consisting of the inner sleeve and the outer shell, while using conventional technique.

5 EP 194 797 describes a cladding tube with an outer component and an inner component intended to protect the cladding against PCI damage. The inner component has a specific composition, zirconium with 0.4-0.6 % tin, 0.5-1.4 % iron and 100-700 ppm oxygen, in order to impart to the inner component good corrosion properties in the event that water  
10 should penetrate into the rod.

The cladding tube is manufactured by processing the ingot of the inner component in a conventional way for the manufacture of Zircaloy, including beta quenching, before the inner  
15 component is joined to the outer component. After the joining of the outer and inner components, the cladding tube can be additionally beta-quenched either before the last cold-rolling step by beta-quenching the outer surface, or before the penultimate rolling step by beta-quenching the  
20 entire cladding wall comprising both the outer and inner components.

EP 155 603 also describes a nuclear fuel element comprising a composite cladding tube with an internal lining of zirconium to avoid cracking in the cladding upon thermal expansion of the pellets. According to this patent specification, it is known to reduce the sensitivity of the zirconium lining to cracking by limiting the total amount of impurities to a level below 5000 ppm and by maintaining the ratio  
25 of the oxygen content to the iron content greater than 1. The manufacture of a zirconium-lined cladding tube is performed by melting zirconium into an ingot which is then forged and shaped into a hollow billet. The hollow billet is inserted into another hollow billet of a zirconium alloy.  
30 The composite billets are heat-extruded into a tube blank. The tube blank is then subjected to repeated cold rolling operations and heat treatments according to conventional tube manufacture. A heat-treatment step consisting of a

solution treatment at 800 or 860°C, near the phase transformation temperature to cause secondary phases in the material to become dissolved, and thereafter a rapid cooling to room temperature as well as a stress-removing heat treatment at a low temperature, for example 550°C for 2 hours, are carried out either after the forging or after the heat extrusion or as a last step on the finished tube, whereby it is considered to be especially effective to carry out the heat treatment as a last step. The best result is achieved according to the specification when the solution treatment is carried out in all the alternative steps during the process.

SE 8903595-0 described a method for manufacturing cladding tubes of zirconium alloy, the outer surface of which is to obtain improved resistance to nodular corrosion during operation in a boiling reactor. The cladding tube is manufactured from a Zr-base alloy and is preferably beta-quenched before extrusion. Before the last cold-rolling step, the outer surface of the tube is beta-quenched. After extrusion, thus, only an outer part of the tube is beta-quenched in order to impart to this part improved corrosion resistance. Such a tube can also be provided with an inner component for PCI protection. After extrusion, the inner component in such a case will not be affected by the beta quenching prior to the last rolling step.

SE 8301770-7 describes a fuel rod comprising a composite cladding tube with an internal layer consisting of sponge zirconium alloyed with 0.1 % tin. This fuel rod exhibits an increased resistance to the corrosive effect of water and water steam at elevated temperature. The cladding tube is manufactured by arranging a tube of the zirconium alloy, constituting the inner component, in a coarser tube of Zircaloy, the end surfaces of the two tubes being welded together. Thereafter, the composite tube is extruded without being subjected to any heating. The extruded product is then cold-rolled in several steps with intermediate recrystallization annealings at about 650°C and is finally annealed after the last cold rolling at about 525°C.

The inner side of the cladding tube can be subjected to the corrosive effect of water and water steam in those cases where damage occurs on the cladding, which may result in water penetrating into the tube. The water will then become evaporated upon contact with the hotter fuel pellets. This results in the inside of the cladding tube being subjected to a corrosive effect of water/water steam of high temperature. When zirconium and zirconium alloys are corroded, hydrogen is formed, which to a certain extent is taken up by the cladding. The hydrogen will be precipitated in the form of zirconium hydrides if the concentration of hydrogen is lower than the saturation concentration of the zirconium. The zirconium hydrides are brittle and have a negative influence on the integrity of the tube. It is therefore of importance that the corrosion and the hydrogen absorption, caused by the corrosion, are as slight as possible in order not to risk that damage involving the penetration of water is extended such that a major quantity of water can penetrate through the tube and leaching of uranium dioxide and radioactive fission products can take place. Damage to a cladding tube can occur for several reasons, for example wear or defects in the welds.

The outer side of a fuel rod is always in contact with water and water steam, and it is known that heat treatments affect zirconium and the resistance of zirconium alloys to corrosion in water and water steam at a high temperature. Thus, a large number of publications describe heat treatments intended to improve the resistance of zirconium alloys to corrosion. EP 71193 describes how, during conventional manufacture, an ingot of a zirconium alloy is first forged in the beta-phase range and thereafter heat-treated in the beta-phase range followed by rapid quenching. Then, the billet is forged in the alpha-phase range and extruded, followed by tube manufacture involving cold-working steps and intermediate annealings in a conventional manner. To improve the corrosion resistance of the tube, it was found that the favourable solution treatment in the beta or alpha+beta-

phase range followed by rapid quenching from the heat treatment temperature should be carried out also at a later stage in the process, after hot extrusion of the billet.

## 5 SUMMARY OF THE INVENTION

According to the present invention, it has proved that a nuclear fuel element can exhibit an improved resistance to the effect of water and water steam in case of damage involving the penetration of water into a fuel rod provided with an internal liner layer by a careful choice, during the manufacture of the cladding tube, of parameters for heat treatment of the inner component from the very machining of an ingot of the inner component.

Surprisingly, it has proved that also the heat treatments during the manufacture of the inner component into a composite cladding tube, which are carried out before the inner component is joined to the outer component to be extruded together, are of great importance for obtaining a fuel element with improved resistance to the corrosive effect of water and water steam and where the harmful hydrogen absorption during the corrosion process is reduced, in the event that a cladding tube is damaged such that water can penetrate through the cladding.

It has also proved, according to the present invention, that by choosing an optimum composition of the liner layer, the effect of manufacture, with chosen heat-treatment parameters for all the heat treatments, can be further improved.

According to the present invention, a fuel element comprising cladding tubes, with an internal layer, is to be manufactured by producing an ingot of zirconium or a zirconium alloy, for example zirconium-tin, suitable as inner layer in a PCI-resistant cladding. The ingot is machined by forging operations and possibly by rolling and extrusion into a suitable dimension to be joined to the outer component. To

obtain optimum properties of the inner component, this component, during all the process steps after the manufacture of the ingot, such as forging, heat treatment, rolling, extrusion, intermediate annealing and final annealing, is to  
5 be maintained at temperatures lower than the temperature at which beta phase starts forming in the inner component.

An incipient transformation of alpha phase into beta phase takes place for zirconium with low oxygen contents, which is  
10 usually used as inner component in a PCI-resistant cladding, at 800°C. For zirconium-tin alloys, which are also used as inner component, tin stabilizes the alpha phase and the transformation temperature lies just above 862°C. During the formation of beta phase, a gradual dissolution of secondary  
15 phases, impurities and precipitated particles in the matrix takes place,

According to the present invention, the inner component should not be heat-treated at temperatures where beta phase  
20 is formed, and secondary phases and impurities should be prevented from dissolving in the matrix. This also applies to the early stage of the manufacturing chain, such as preheating, preliminary forging, and final forging.

25 For the manufacture of a nuclear fuel element according to the invention, an ingot is manufactured from the inner component. Ingots of zirconium are heat-treated in the alpha-phase range at 700-800°C and ingots of a zirconium-tin alloy are heat-treated in the alpha-phase range at 700-  
30 860°C before being forged. After that, a repeated forging operation with preheating within the same temperature interval in the alpha-phase range can take place. It is thus important that also the preliminary forging of the ingot  
35 take place at a temperature below the temperature at which an incipient transformation to beta phase takes place. An advantage of zirconium-tin alloys is that these can be heated to a higher temperature before the phase transformation takes place, which facilitates the machining of the



ingot. Additional machining of the inner component, to obtain a suitable dimension of the inner component for joining to the outer component, is suitably carried out by hot rolling and extrusion. The temperature of the inner component should not exceed 710°C during these process stages.

A further improvement of the corrosion resistance of the inner component can be obtained by introducing additional heat treatment of a billet of the inner component in addition to the heat treatments which take place in connection with forging, rolling and/or extrusion, before it is joined to the outer component. This additional heat treatment is carried out in the alpha-phase range at 600-800°C for billets of zirconium and 600-860°C for billets of zirconium-tin alloy and preferably within the interval 650-750°C, irrespective of the composition of the billet. This extra heat treatment can be carried out as a last step before the inner component is joined to the outer component or earlier in the process chain, for example before the inner component is extruded.

When the inner component has been machined into a suitable dimension, it can be joined to the outer component by passing a tube of the inner component into a coarser tube of the outer component in a conventional way.

The outer component consists of a zirconium alloy intended to constitute a supporting part of a composite cladding tube, for example Zircaloy 2 and Zircaloy 4, whose contents of alloying materials lie within the limits 1.2-1.7% tin, 0.07-0.24% iron, 0.05-0.15% chromium and 0-0.08% nickel, the balance being zirconium and any impurities of a conventional kind or Zr 2.5 Nb. The outer component is machined in a conventional way by forging in the beta or alpha+beta-phase range followed by forging in the alpha-phase range and further degradation by forging and extrusion (if any). Before the outer component is joined to the inner component,

the billet is beta-quenched by heating to the beta-phase range, for example 1050°C, and is thereafter rapidly cooled.

5 The composite billet consisting of an inner component and an outer component, is extruded at a temperature below 710°C.

10 After the extrusion, the tube blank is machined in a conventional way by means of a number of cold rolling steps with intermediate heat-treatment operations and a final heat treatment. Intermediate heat treatments of the inner component are performed within the interval 525-700°C and the final heat treatment is performed within the interval 400-700°C.

15 For the manufacture of a fuel element with cladding tubes with inner layers of zirconium, an extra heat treatment of the tube blank can be carried out after the inner component has been joined to the outer component. This heat treatment is carried out at in the alpha-phase range, suitably at 600-  
20 800°C. The limited diffusion of alloying materials which can take place between the outer component and the inner component during the heat treatment is not harmful to the PCI resistance of the layer. To ensure that a heat treatment of this kind does not have an adverse effect on the corrosion  
25 properties of the outer component, the outer part of the tube can be beta-quenched after the extra heat treatment has been carried out. During beta quenching, the outer part of the tube is heated to a temperature in the beta-phase range, for example 1050°C and is then rapidly cooled.

30 The inner component can consist of pure zirconium or consist of a zirconium-tin alloy with 0.1 to 1% tin, such as an alloy of zirconium with 0.1-0.5% tin and with an iron content less than 550 ppm, preferably 200-450 ppm and less  
35 than 600 ppm oxygen. Impurities in zirconium and a zirconium-tin alloy shall be below the limits which normally apply to reactor-grade zirconium, namely, Al 75 ppm, B 0.5 ppm, C 100 ppm, Ca 30 ppm, Cd 0.5 ppm, Cl 20 ppm, Co 20 ppm,

Cu 50 ppm, H 25 ppm, Hf 100 ppm, Mg 20 ppm, Mn 50 ppm, Mo 50 ppm, N 65 ppm, Na 20 ppm, Nb 100 ppm, Ni 70 ppm, P 30 ppm, Pb 100 ppm, Si 100 ppm, Ta 200 ppm, Ti 50 ppm, U 3.5 ppm, V 50 ppm, W 100 ppm and Cr 200 ppm.

5

The inner component can also consist of other zirconium alloys.

10

The invention will be explained in greater detail by description of an embodiment with reference to the accompanying figure which shows a flow diagram for the manufacture of a cladding tube.

15

An ingot of the inner component is manufactured (1). The inner component consists of zirconium with 0.25% Sn, 310 ppm Fe and 430 ppm O as well as impurity quantities normally occurring in reactor-grade zirconium. Thereafter, the ingot is preheated (2) and forged (3). These steps can be repeated by preliminary forging and finally forging the ingot. The ingot is preheated to a temperature of 820°C for 8 hours (2) and is forged (3), whereupon an additional heating to 800°C (2) and a final forging (3) are carried out. After forging, the billet is rolled down (4) and extruded at a temperature of about 670°C (5). Thereafter, the billet is annealed at 650°C for 5 hours (6).

30

The outer component is manufactured conventionally by forging and is beta-quenched before extrusion (7, 8, 9, 10, 11).

35

The inner component is joined to the outer component in conventional manner and the composite body is extruded (12) at a temperature of about 670°C. Thereafter, the tube blank is rolled in three stages into the final dimension with intermediate annealings at 570°C for 1 hour (13, 14). After the last rolling, the tube is finally annealed at 570°C for 1.5 hours (15).

The cladding tubes are filled with fuel pellets and sealed, whereupon they are assembled into bundles forming nuclear fuel elements intended for light-water reactors.

## CLAIMS

1. A method for manufacturing a nuclear fuel element comprising a composite cladding tube with an inner component of  
5 zirconium or a zirconium alloy suitable as inner component in a PCI-resistant composite cladding as well as an outer component of a zirconium alloy intended to constitute the supporting part of a composite cladding tube, such as, for example, Zircaloy 2, Zircaloy 4 or Zr 2.5 Nb, wherein the  
10 cladding tube is manufactured by fabricating an ingot of the composition of the inner component and an ingot of the composition of the outer component, respectively, and machining them separately into a billet of a suitable dimension and thereafter joining them together and extruding to a tube  
15 blank and machining it further by means of cold rolling and intermediate heat-treatment operations and a final heat treatment in the final dimension, characterized in that the inner component of zirconium or a zirconium alloy during the manufacture, from the production of an ingot up to the  
20 completion of a cladding tube, comprising forging, rolling, extrusion, heat treatment and final heat treatment, is only subjected to heat influence at temperatures in the alpha-phase range below the temperature when an incipient beta-phase transformation takes place.
- 25 2. A method according to claim 1, characterized in that the inner component is preheat-treated before the forging at a temperature in the alpha-phase range.
- 30 3. A method according to claim 2, characterized in that the inner component is forged in two steps and that the preheat treatment before said steps is carried out at a temperature in the alpha-phase range.
- 35 4. A method according to claim 1, characterized in that the inner component is manufactured from a zirconium-tin alloy comprising zirconium with 0.1-1 % tin and preferably zirconium with 0.1-0.5 % tin and less than 600 ppm iron,

preferably 200-450 ppm iron, and less than 600 ppm oxygen, as well as contents of impurities below the limits which normally apply to reactor-grade zirconium.

- 5 5. A method according to claims 1 and 2, characterized in that an ingot of material intended to constitute the inner component is preheated at 700-860°C before forging of the ingot.
- 10 6. A method according to claims 1, 2 and 3, characterized in that the billet is rolled and/or extruded at a temperature below 710°C.
- 15 7. A method according to claims 1, 2, 3 and 4, characterized in that the billet is heat-treated, in addition to the heat-treatment operations which are performed in connection with forging, rolling and/or extrusion, at 600-860°C, preferably at 650-750°C.
- 20 8. A method according to claim 1, characterized in that the inner component is manufactured from zirconium with impurity contents below those which normally apply to reactor-grade zirconium.
- 25 9. A method according to claims 1 and 6, characterized in that an ingot of material intended to constitute the inner component is preheated to 700-800°C before forging of the ingot.
- 30 10. A method according to claims 1, 6 and 7, characterized in that the billet is rolled and/or extruded at a temperature below 710°C.
- 35 11. A method according to claims 1, 6, 7 and 8, characterized in that the billet is heat-treated, in addition to the heat-treatment operations which are performed in connection with forging, rolling and/or extrusion, at 600-800°C, preferably at 650-750°C.

12. A method according to one or more of the preceding claims, characterized in that extrusion takes place at a temperature below 710°C.
- 5 13. A method according to one or more of the preceding claims, characterized in that the extruded tube blank is cold-rolled in a number of steps with intermediate heat-treatment operations at 525-700°C and is finally heat-treated at 400- 700°C.
- 10 14. A method according to one or more of the preceding claims, characterized in that, after extrusion, a heat treatment is carried out at 600-800°C and that, after this heat treatment, a beta quenching of the outer part of the
- 15 cladding tube is carried out.

## AMENDED CLAIMS

[received by the International Bureau on 16 May 1994 (16.05.94);  
original claims 1-14 replaced by amended claims 1-14 (3 pages)]

1. A method for manufacturing a nuclear fuel element comprising a composite cladding tube with an inner component of  
5 zirconium or a zirconium alloy suitable as inner component in a PCI-resistant composite cladding as well as an outer component of a zirconium alloy intended to constitute the supporting part of a composite cladding tube, such as, for example, Zircaloy 2, Zircaloy 4 or Zr 2.5 Nb, wherein the  
10 cladding tube is manufactured by fabricating an ingot of the composition of the inner component and an ingot of the composition of the outer component, respectively, and machining them separately into a billet of a suitable dimension and thereafter joining them together and extruding to a tube  
15 blank and machining it further by means of cold rolling and intermediate heat-treatment operations and a final heat treatment in the final dimension, characterized in that the inner component of zirconium or a zirconium alloy during the manufacture, from the production of an ingot up to the  
20 completion of a cladding tube, comprising forging, rolling, extrusion, heat treatment and final heat treatment, is only subjected to heat influence at temperatures in the alpha-phase range below the temperature when an incipient beta-phase transformation takes place.
- 25
2. A method according to claim 1, characterized in that the inner component is preheat-treated before the forging at a temperature in the alpha-phase range.
- 30
3. A method according to claim 2, characterized in that the inner component is forged in two steps and that the preheat treatment before said steps is carried out at a temperature in the alpha-phase range.
- 35
4. A method according to claim 1, 2 or 3, characterized in that the inner component is manufactured from a zirconium-tin alloy comprising zirconium with 0.1-1 % tin and preferably zirconium with 0.1-0.5 % tin and less than 600 ppm iron, preferably 200-450 ppm iron, and less than 600 ppm oxygen,



as well as contents of impurities below the limits which normally apply to reactor-grade zirconium.

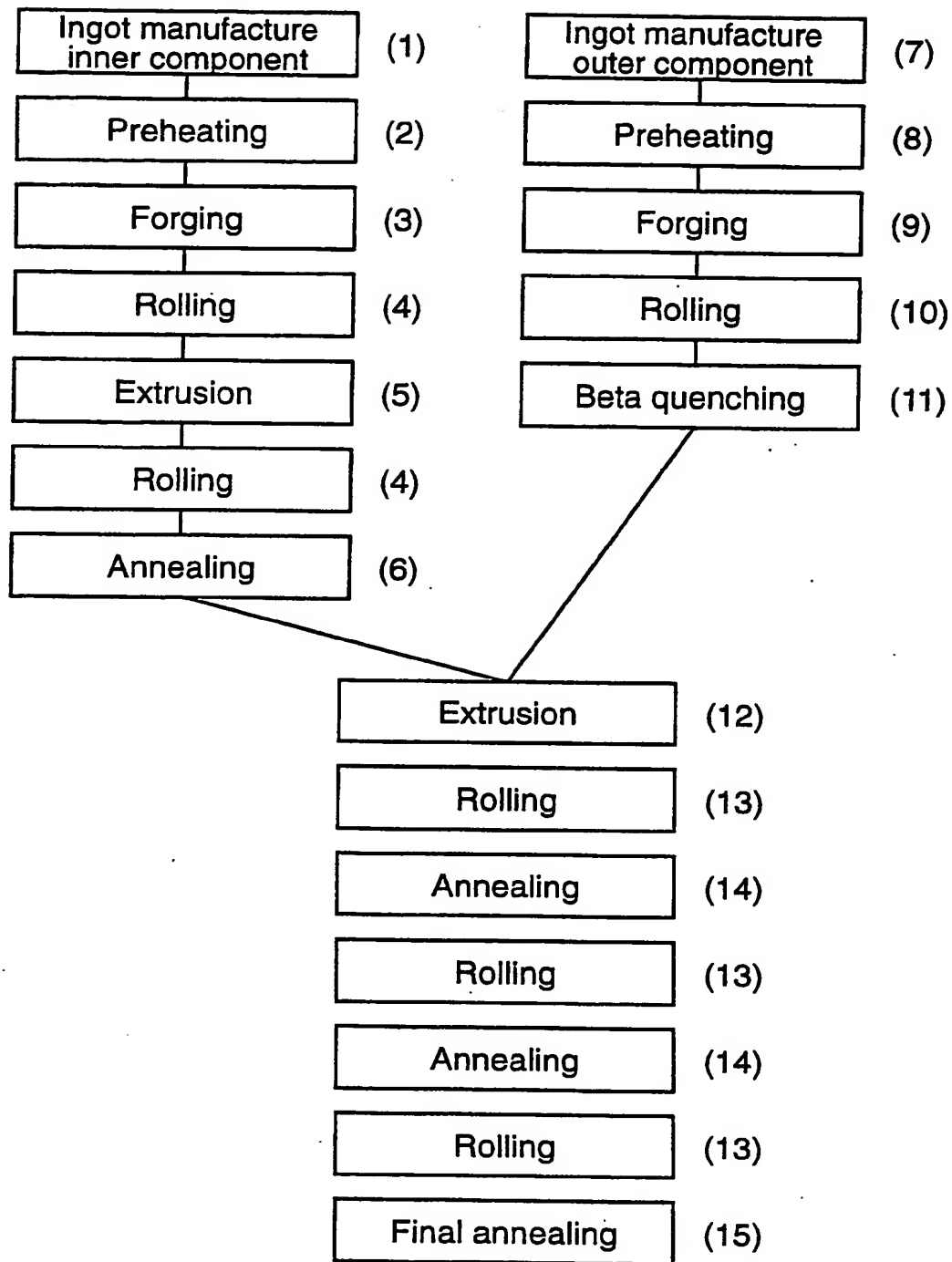
- 5 5. A method according to claim 4, characterized in that an ingot of material intended to constitute the inner component is preheated at 700-860°C before forging of the ingot.
- 10 6. A method according to claim 4 or 5, characterized in that the blank is heat-treated, in addition to the heat-treatment operations which are performed in connection with forging, rolling and/or extrusion, at 600- 860°C, preferably at 650-750°C.
- 15 7. A method according to claim 1, characterized in that the inner component is manufactured from zirconium with impurity contents below those which normally apply to reactor-grade zirconium.
- 20 8. A method according to claim 7, characterized in that an ingot of material intended to constitute the inner component is preheated to 700-800°C before forging of the ingot.
- 25 9. A method according to claim 7 or 8, characterized in that the billet is heat-treated, in addition to the heat-treatment operations which are performed in connection with forging, rolling and/or extrusion, at 600- 800°C, preferably at 650-750°C.
- 30 10. A method according to one or more of the preceding claims, characterized in that coextrusion takes place at a temperature below 710°C.
- 35 11. A method according to any of the preceding claims, characterized in that the billet of the inner component is rolled and/or extruded at a temperature below 710°C.
12. A method according to one or more of the preceding claims, characterized in that the extruded tube blank is cold-rolled in a number of steps with intermediate heat-

treatment operations at 525-700°C and is finally heat-treated at 400- 700°C.

13. A method according to one or more of the preceding  
5 claims, characterized in that, after extrusion, a heat treatment is carried out at 600-800°C.

14. A method according to claim 13, characterized in that  
10 an outer part of the cladding tube blank is beta quenched after the heat treatment according to claim 13.

1/1



1  
INTERNATIONAL SEARCH REPORT

International application No.

PCT/SE 93/01070

**A. CLASSIFICATION OF SUBJECT MATTER**

IPC5: G21C 21/02, G21C 3/20

According to International Patent Classification (IPC) or to both national classification and IPC

**B. FIELDS SEARCHED**

Minimum documentation searched (classification system followed by classification symbols)

IPC5: G21C

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

SE,DK,FI,NO classes as above

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

**C. DOCUMENTS CONSIDERED TO BE RELEVANT**

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
Y	EP, A1, 0194797 (WESTINGHOUSE ELECTRIC CORPORATION), 17 Sept 1986 (17.09.86), page 5, line 19 - line 27; page 6, line 24 - page 8, line 24	1-14
Y	EP, A1, 0425465 (SANDVIK AKTIEBOLAG), 2 May 1991 (02.05.91), page 3, line 40 - line 54; page 4, line 13 - line 19	1-14
A	EP, A1, 0155603 (NIPPON NUCLEAR FUEL DEVELOPMENT CO., LTD), 25 Sept 1985 (25.09.85), page 15, line 8 - line 19; page 16, line 18 - page 17, line 9, figure 6	1,8

☒ Further documents are listed in the continuation of Box C.

☒ See patent family annex.

\* Special categories of cited documents:

- "A" document defining the general state of the art which is not considered to be of particular relevance
- "E" earlier document but published on or after the international filing date
- "L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)
- "O" document referring to an oral disclosure, use, exhibition or other means
- "P" document published prior to the international filing date but later than the priority date claimed

"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention

"X" document of particular relevance: the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone

"Y" document of particular relevance: the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art

"&" document member of the same patent family

Date of the actual completion of the international search

24 March 1993

Date of mailing of the international search report

28 -03- 1994

Name and mailing address of the ISA/  
Swedish Patent Office  
Box 5055, S-102 42 STOCKHOLM  
Facsimile No. +46 8 666 02 86

Authorized officer

Peter Thomasson  
Telephone No. +46 8 782 25 00

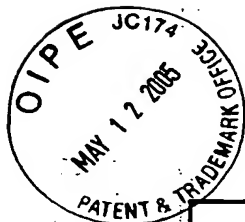
2  
INTERNATIONAL SEARCH REPORT

International application No.

PCT/SE 93/01070

C (Continuation). DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	EP, A1, 0121204 (AB ASEA-ATOM), 10 October 1984 (10.10.84), page 5, line 7 - line 23  --	1,8
A	SE, B, 459340 (COMPAGNIE EUROPEENNE DU ZIRCONIUM CEZUS COURBEVOIE FR), 26 June 1989 (26.06.89), abstract  -----	1



**INTERNATIONAL SEARCH REPORT**  
Information on patent family members

26/02/94

International application No.

PCT/SE 93/01070

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
EP-A1- 0194797	17/09/86	SE-T3- 0194797 JP-C- 1766149 JP-B- 4057237 JP-A- 61207989	11/06/93 10/09/92 16/09/86
EP-A1- 0425465	02/05/91	JP-A- 3209191 SE-B, C- 463790 SE-A- 8903595	12/09/91 21/01/91 21/01/91
EP-A1- 0155603	25/09/85	SE-T3- 0155603 JP-A- 60190888 US-A- 4863679 JP-B- 4041794 JP-A- 60190889 JP-C- 1697681 JP-B- 3065873 JP-A- 60190891	28/09/85 05/09/89 09/07/92 28/09/85 28/09/92 15/10/91 28/09/85
EP-A1- 0121204	10/10/84	JP-C- 1702220 JP-B- 3071078 JP-A- 59184882 SE-A- 436078 US-A- 4610842	14/10/92 11/11/91 20/10/84 05/11/84 09/09/86
SE-B- 459340	26/06/89	DE-A, C- 3609074 FR-A, B- 2579122 GB-A, B- 2172737 JP-C- 1534308 JP-A- 61213362 SE-A- 8601240	02/10/86 26/09/86 24/09/86 12/12/89 22/09/86 20/09/86

**This Page is Inserted by IFW Indexing and Scanning  
Operations and is not part of the Official Record**

**BEST AVAILABLE IMAGES**

Defective images within this document are accurate representations of the original documents submitted by the applicant.

Defects in the images include but are not limited to the items checked:

- ☒ BLACK BORDERS
- ☒ IMAGE CUT OFF AT TOP, BOTTOM OR SIDES
- ☒ FADED TEXT OR DRAWING
- ☐ BLURRED OR ILLEGIBLE TEXT OR DRAWING
- ☒ SKEWED/SLANTED IMAGES
- ☒ COLOR OR BLACK AND WHITE PHOTOGRAPHS
- ☒ GRAY SCALE DOCUMENTS
- ☐ LINES OR MARKS ON ORIGINAL DOCUMENT
- ☐ REFERENCE(S) OR EXHIBIT(S) SUBMITTED ARE POOR QUALITY
- ☐ OTHER: \_\_\_\_\_

**IMAGES ARE BEST AVAILABLE COPY.**

**As rescanning these documents will not correct the image problems checked, please do not report these problems to the IFW Image Problem Mailbox.**

**This Page Blank (uspto)**